## 40V, 3A Synchronous Step-Down COT Power Module

## Description

The XR79203 is part of a family of 40V synchronous step-down power modules combining the controller, drivers, inductor, passive components and MOSFETs in a single package for point-of-load supplies. This module requires very few external components leading to ease of design and fast time to market. The XR79203 has load current rating of 3 A . A wide 5 V to 40 V input voltage range allows for single supply operation from industry standard $24 \mathrm{~V} \pm 10 \%, 18 \mathrm{~V}$ to 36 V and rectified 18VAC and 24VAC rails.

With a proprietary emulated current mode Constant On-Time (COT) control scheme, the XR79203 provides extremely fast line and load transient response using ceramic output capacitors. It requires no loop compensation, simplifying circuit implementation and reducing overall component count. The control loop also provides $0.1 \%$ load and $0.2 \%$ line regulation and maintains constant operating frequency. A selectable power saving mode, allows the user to operate in Discontinuous Current Mode (DCM) at light current loads significantly increasing the converter efficiency.

A host of protection features, including overcurrent, over temperature, short-circuit and UVLO, helps achieve safe operation under abnormal operating conditions.
The XR79203 is available in a RoHS-compliant, green/halogen-free space-saving $8 \mathrm{~mm} \times 8 \mathrm{~mm} \times 4 \mathrm{~mm}$ QFN package.

## Typical Application



Figure 1. Typical Application

## FEATURES

- 3A step-down power module - 5 V to 40 V wide single input voltage
- $\geq 0.6 \mathrm{~V}$ adjustable output voltage
- Controller, drivers, inductor, passive components and MOSFETs integrated in one package
- Proprietary constant on-time control
- No loop compensation required
- Stable with ceramic output capacitors
- Programmable 100 ns - $1 \mu$ s on-time
- Constant 400 kHz to 800 kHz frequency
- Selectable CCM or DCM/CCM operation
- Precision enable and power-good flag
- Programmable soft-start
- $8 \mathrm{~mm} \times 8 \mathrm{~mm} \times 4 \mathrm{~mm}$ QFN package


## APPLICATIONS

- Drones and remote vehicles
- Automotive displays
- FPGA/DSP/processor supplies
- Industrial control and automation
- Telecommunications and infrastructure equipment
- Distributed power architecture


Figure 2. Efficiency, $24 \mathrm{~V}_{\mathrm{IN}}$

## Absolute Maximum Ratings

These are stress ratings only and functional operation of the device at these ratings or any other above those indicated in the operation sections of the specifications below is not implied. Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. Exposure to any absolute maximum rating condition for extended periods may affect device reliability and lifetime.
$\mathrm{V}_{\mathrm{CC}}$............................................................................ -0.3 V to 6.0 V
BST............................................................... 0.3 V to 48V ${ }^{(1)}$
BST-SW............................................................. -0.3V to 6V
SW, ILIM........................................................ -1V to 43V ${ }^{(1)(2)}$
All other pins........................................ -0.3 V to $\mathrm{V}_{\mathrm{CC}}+0.3 \mathrm{~V}$
Storage temperature................................... $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Junction temperature................................................. $150^{\circ} \mathrm{C}$
Power dissipation ...................................... Internally limited
Lead temperature (soldering, 10 seconds)................ $300^{\circ} \mathrm{C}$
ESD rating (HBM - human body model) ....................... 2 kV
ESD rating (CDM - charged device model) .................. 2 kV

## Operating Conditions


SW, ILIM .................................................... -1V to 40V ${ }^{(1)(2)}$
PGOOD, $\mathrm{V}_{\mathrm{CC}}$, TON, SS, EN, FB................... -0.3V to 5.5 V
Switching frequency ........................... 400 kHz to $800 \mathrm{kHz}{ }^{(3)}$
Junction temperature range ( $\mathrm{T}_{\mathrm{J}}$ ) $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$
Package power dissipation max at $25^{\circ} \mathrm{C}$
4.3W

Package thermal resistance $\theta_{\mathrm{JA}} \ldots . . . . . . . . . . . . . . . . . . . . . . . . . . .23^{\circ} \mathrm{C} / \mathrm{W}$
Notes:

1. No external voltage applied.
2. SW pin's $D C$ range is -1 V , transient is -5 V for less than 50 ns .
3. Recommended frequency for optimum performance.

## Electrical Characteristics

$\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}$, BST $=\mathrm{V}_{\mathrm{CC}}$, $\mathrm{SW}=\mathrm{AGND}=\mathrm{PGND}=0 \mathrm{~V}, \mathrm{C}_{\mathrm{VCC}}=4.7 \mu \mathrm{~F}$, unless otherwise specified. Limits applying over the full operating temperature range are denoted by $a^{\bullet}$.

| Symbol | Parameter | Conditions | - | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Power Supply Characteristics |  |  |  |  |  |  |  |
| $\mathrm{V}_{\text {IN }}$ | Input voltage range | $\mathrm{V}_{\mathrm{CC}}$ regulating | - | 5 |  | 40 | V |
| IVin | $\mathrm{V}_{\text {IN }}$ supply current | Not switching, $\mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=0.7 \mathrm{~V}$ | - |  | 0.7 | 2 | mA |
|  |  | $\mathrm{f}=500 \mathrm{kHz}, \mathrm{R}_{\mathrm{ON}}=124 \mathrm{k} \Omega, \mathrm{V}_{\mathrm{FB}}=0.58 \mathrm{~V}$ |  |  | 10 |  | mA |
| Ioff | Shutdown current | Enable $=0 \mathrm{~V}, \mathrm{P}_{\mathrm{VIN}}=\mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}$ |  |  | 1 |  | $\mu \mathrm{A}$ |
| Enable and Undervoltage Lock-Out (UVLO) |  |  |  |  |  |  |  |
| VIH_EN_1 | EN pin rising threshold |  | - | 1.8 | 1.9 | 2.0 | V |
| VEN_HYS_1 | EN pin hysteresis |  |  |  | 70 |  | mV |
| $\mathrm{V}_{\text {IH_EN_2 }}$ | EN pin rising threshold for DCM/ CCM |  | - | 2.8 | 3.0 | 3.1 | V |
| $\mathrm{V}_{\text {EN_HYS_2 }}$ | EN pin hysteresis |  |  |  | 110 |  | mV |
|  | $\mathrm{V}_{\mathrm{CC}}$ UVLO start threshold | Rising edge | - | 4.00 | 4.25 | 4.40 | V |
|  | $\mathrm{V}_{\mathrm{CC}}$ UVLO hysteresis |  | - |  | 195 |  | mV |

## Electrical Characteristics (Continued)

$\mathrm{T}_{J}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}, \mathrm{BST}=\mathrm{V}_{\mathrm{CC}}, \mathrm{SW}=\mathrm{AGND}=\mathrm{PGND}=0 \mathrm{~V}, \mathrm{C}_{\mathrm{VCC}}=4.7 \mu \mathrm{~F}$, unless otherwise specified. Limits applying over the full operating temperature range are denoted by $\mathrm{a} \cdot$.

| Symbol | Parameter | Conditions | - | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Reference Voltage |  |  |  |  |  |  |  |
| $\mathrm{V}_{\text {REF }}$ | Reference voltage | $\mathrm{V}_{I N}=5 \mathrm{~V}$ to 40V, $\mathrm{V}_{\text {CC }}$ regulating |  | 0.596 | 0.600 | 0.604 | V |
|  |  |  | - | 0.594 | 0.600 | 0.606 | V |
|  | DC load regulation | CCM operation, closed loop, applies to any Cout |  |  | $\pm 0.1$ |  | \% |
|  | DC line regulation |  |  |  | $\pm 0.2$ |  | \% |
| Programmable Constant On-Time |  |  |  |  |  |  |  |
| ton(MIN) | Minimum programmable on-time | $\mathrm{R}_{\mathrm{ON}}=14 \mathrm{k} \Omega, \mathrm{V}_{\text {IN }}=40 \mathrm{~V}$ |  |  | 120 |  | ns |
| ton 1 | On-time 1 | $\mathrm{R}_{\text {ON }}=14 \mathrm{k} \Omega, \mathrm{V}_{\text {IN }}=24 \mathrm{~V}$ | - | 180 | 200 | 220 | ns |
| ton2 | On-time 2 | $\mathrm{R}_{\text {ON }}=35.7 \mathrm{k} \Omega, \mathrm{V}_{\text {IN }}=24 \mathrm{~V}$ | - | 420 | 470 | 520 | ns |
|  | On-time 2 frequency | $\mathrm{R}_{\text {ON }}=35.7 \mathrm{k} \Omega, \mathrm{V}_{\text {IN }}=24 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=5.0 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=3 \mathrm{~A}$ |  | 425 | 470 | 525 | kHz |
| Toff(MIN) | Minimum off-time |  | - |  | 250 | 350 | ns |
| Diode Emulation Mode |  |  |  |  |  |  |  |
|  | Zero crossing threshold | DC value measured during test |  |  | -2 |  | mV |
| Soft-Start |  |  |  |  |  |  |  |
|  | SS charge current |  | - | -14 | -10 | -6 | $\mu \mathrm{A}$ |
|  | SS discharge current | Fault present | - | 1 |  |  | mA |
| $\mathrm{V}_{\text {CC }}$ Linear Regulator |  |  |  |  |  |  |  |
|  | $\mathrm{V}_{\mathrm{CC}}$ output voltage | $\mathrm{V}_{\mathrm{IN}}=6 \mathrm{~V}$ to 40 V , $\mathrm{I}_{\text {LOAD }}=0$ to 30 mA | - | 4.8 | 5.0 | 5.2 | V |
|  |  | $\mathrm{V}_{\mathrm{IN}}=5 \mathrm{~V}$, $\mathrm{I}_{\text {LOAD }}=0$ to 20 mA | - | 4.51 | 4.8 |  |  |
| Power Good Output |  |  |  |  |  |  |  |
|  | Power good threshold |  |  | -10 | -7 | -5 | \% |
|  | Power good hysteresis |  |  |  | 1.5 | 4 | \% |
|  | Power good sink current |  |  | 1 |  |  | mA |

## Electrical Characteristics (Continued)

$\mathrm{T}_{J}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}, \mathrm{BST}=\mathrm{V}_{\mathrm{CC}}, \mathrm{SW}=\mathrm{AGND}=\mathrm{PGND}=0 \mathrm{~V}, \mathrm{C}_{\mathrm{VCC}}=4.7 \mu \mathrm{~F}$, unless otherwise specified. Limits applying over the full operating temperature range are denoted by a $\bullet$.

| Symbol | Parameter | Conditions | - | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Protection: OCP, OTP, Short-Circuit |  |  |  |  |  |  |  |
|  | Hiccup timeout |  |  |  | 110 |  | ms |
|  | $\mathrm{ILIM}^{\prime} / \mathrm{R}_{\text {DS }}$ |  |  | 2.40 | 2.85 | 3.20 | $\mu \mathrm{A} / \mathrm{m} \Omega$ |
|  | lıIM current temperature coefficient |  |  |  | 0.4 |  | \%/ ${ }^{\circ} \mathrm{C}$ |
|  | ІІІм comparator offset |  | - | -8 | 0 | 8 | mV |
|  | Current limit blanking | GL rising > 1V |  |  | 100 |  | ns |
|  | Thermal shutdown threshold | Rising temperature |  |  | 150 |  | ${ }^{\circ} \mathrm{C}$ |
|  | Thermal hysteresis |  |  |  | 15 |  | ${ }^{\circ} \mathrm{C}$ |
|  | Feedback pin short-circuit threshold | Percent of $\mathrm{V}_{\text {REF }}$, short-circuit is active. After PGOOD is asserted | - | 50 | 60 | 70 | \% |
| Output Power Stage |  |  |  |  |  |  |  |
| $\mathrm{R}_{\text {DSON }}$ | High-side MOSFET | $I_{\text {DS }}=2 A$ |  |  | 41 | 59 | $\mathrm{m} \Omega$ |
|  | Low-side MOSFET |  |  |  | 17 | 21.5 | $\mathrm{m} \Omega$ |
| Iout | Maximum output current |  | - | 3 |  |  | A |
| L | Output inductance |  |  | 3.7 | 4.7 | 5.6 | $\mu \mathrm{H}$ |
| $\mathrm{Cl}_{\text {IN }}$ | Input capacitance |  |  |  | 1 |  | $\mu \mathrm{F}$ |
| $\mathrm{C}_{\text {BST }}$ | Bootstrap capacitance |  |  |  | 0.1 |  | $\mu \mathrm{F}$ |

## Pin Configuration



## Pin Functions

## Pin Number Pin Name Type Description

| 1 | SS | A | Soft-start pin. Connect an external capacitor between SS and AGND to program the soft-start rate based on the $10 \mu \mathrm{~A}$ internal source current. |
| :---: | :---: | :---: | :---: |
| 2 | PGOOD | OD, O | Power-good output. This open-drain output is pulled low when $\mathrm{V}_{\text {OUT }}$ is outside the regulation. |
| 3 | FB | A | Feedback input to feedback comparator. Connect with a set of resistors to VOUT and AGND in order to program Vout. |
| $\begin{aligned} & \hline 4,5,53,54, \\ & \text { AGND Pad } \end{aligned}$ | AGND | A | Analog ground. Control circuitry of the IC is referenced to this pin. Connect to PGND. |
| 6 | VIN | PWR | IC supply input. Provides power to internal LDO. Connect to PVIN pins. |
| 7 | VCC | PWR | The output of LDO. Bypass with a $4.7 \mu \mathrm{~F}$ capacitor to AGND. |
| 8 | PGND | PWR | Controller low-side driver ground. Connect with a short trace to closest PGND pins or PGND pad. |
| $\begin{aligned} & \text { 13-19, 39-43, } \\ & \text { PGND Pad } \end{aligned}$ | PGND | PWR | Ground of the power stage. Should be connected to the system's power ground plane. |
| $\begin{gathered} \text { 9-12, 20-23, } \\ \text { SW Pad } \end{gathered}$ | SW | PWR | Switching node. It internally connects the source of the high-side FET, the drain of the low-side FET, the inductor and bootstrap capacitor. Use thermal vias and/or sufficient PCB land area in order to heatsink the low-side FET and the inductor. |
| 24-38, VOUT Pad | VOUT | PWR | Output of the power stage. Place the output filter capacitors as close as possible to these pins. |
| 45-49, PVIN Pad | PVIN | PWR | Power stage input voltage. Place the input filter capacitors as close as possible to these pins. |
| 50, 51, BST Pad | BST | A | Controller high-side driver supply pin. It is internally connected to SW via a $0.1 \mu \mathrm{~F}$ bootstrap capacitor. Leave these pins floating. |
| 52 | ILIM | A | Overcurrent protection programming. Connect with a short trace to SW pins. |
| 55 | EN/MODE | 1 | Precision enable pin. Pulling this pin above 1.9 V will turn the IC on and it will operate in forced CCM. If the voltage is raised above 3.0V, then the IC will operate in DCM or CCM depending on load. |
| 56 | TON | A | Constant on-time programming pin. Connect with a resistor to AGND. |

## NOTE:

$\mathrm{A}=$ Analog, $\mathrm{I}=$ Input, $\mathrm{O}=$ Output, $\mathrm{OD}=$ Open Drain, $\mathrm{PWR}=$ Power.

## Typical Performance Characteristics

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\text {IN }}=24 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=3.3 \mathrm{~V}$, $\mathrm{I}_{\text {OUT }}=3 \mathrm{~A}, \mathrm{f}=500 \mathrm{kHz}$, unless otherwise specified. Schematic shown in Figure 27.


Figure 3. Load Regulation


Figure 5. $\mathrm{t}_{\mathrm{ON}} \mathrm{vs}$. $\mathrm{R}_{\mathrm{ON}}$


Figure 7. Switching Frequency vs. Iout


Figure 4. Line Regulation


Figure 6. $\mathrm{t}_{\mathrm{ON}} \mathrm{vs}$. $\mathrm{V}_{\mathrm{IN}}, \mathrm{R}_{\mathrm{ON}}=14 \mathrm{k} \Omega$


Figure 8. Switching Frequency vs. $\mathrm{V}_{\mathrm{IN}}$

## Typical Performance Characteristics (Continued)

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=3.3 \mathrm{~V}$, $\mathrm{I}_{\mathrm{OUT}}=3 \mathrm{~A}, \mathrm{f}=500 \mathrm{kHz}$, unless otherwise specified. Schematic shown in Figure 27.


Figure 9. loce vs. R


Figure 11. $\mathrm{t}_{\mathrm{ON}} \mathrm{vs}$. Temperature, $\mathrm{R}_{\mathrm{ON}}=14 \mathrm{k} \Omega$


Figure 13. Inductor Current Ripple vs. V


Figure 10. $\mathrm{V}_{\text {REF }}$ vs. Temperature


Figure 12. Inductance vs. Current

## Typical Performance Characteristics (Continued)

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\text {IN }}=24 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=3.3 \mathrm{~V}$, $\mathrm{I}_{\text {OUT }}=3 \mathrm{~A}, \mathrm{f}=500 \mathrm{kHz}$, unless otherwise specified. Schematic shown in Figure 27.


Figure 14. Steady State CCM, IOUT $=3 \mathrm{~A}$


Figure 16. Power Up, $\mathrm{I}_{\text {OUT }}=3 \mathrm{~A}$


Figure 18. Load Step, CCM, OA-1.5A-0A


Figure 15. Steady State DCM, IOUT $=0 \mathrm{~A}$


Figure 17. Power Up, $\mathrm{I}_{\text {OUT }}=\mathrm{OA}$


Figure 19. Load Step, DCM/CCM, 0.05A-1.5A-0.05A

## Typical Performance Characteristics (Continued)

## Efficiency and Package Thermal Derating

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, No airflow, $\mathrm{f}=500 \mathrm{kHz}$, unless otherwise specified. Schematic shown in Figure 27.


Figure 20. Efficiency, $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$


Figure 22. Efficiency, $\mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}$


Figure 21. Maximum $\mathrm{T}_{\text {AMBIENT }}$ vs. I IOUT, $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$


Figure 23. Maximum $\mathrm{T}_{\text {AMbient }}$ vs. lout,

$$
V_{I N}=24 \mathrm{~V}
$$

Functional Block Diagram


Figure 24. Functional Block Diagram

## Applications Information

## Functional Description

XR79203 is a synchronous step-down proprietary emulated current-mode Constant On-Time (COT) module. The on-time, which is programmed via $R_{O N}$, is inversely proportional to $\mathrm{V}_{\mathrm{IN}}$ and maintains a nearly constant frequency. The emulated current-mode control is stable with ceramic output capacitors.
Each switching cycle begins with GH signal turning on the high-side (switching) FET for a preprogrammed time. At the end of the on-time, the high-side FET is turned off and the low-side (synchronous) FET is turned on for a preset minimum time (250ns nominal). This parameter is termed minimum off-time. After the minimum off-time, the voltage at the feedback pin FB is compared to an internal voltage ramp at the feedback comparator. When $\mathrm{V}_{\mathrm{FB}}$ drops below the ramp voltage, the high-side FET is turned on and the cycle repeats. This voltage ramp constitutes an emulated current ramp and makes possible the use of ceramic capacitors, in addition to other capacitor types, for output filtering.

## Enable/Mode Input (EN/MODE)

EN/MODE pin accepts a tri-level signal that is used to control turn on/off. It also selects between two modes of operation: forced CCM and DCM/CCM. If EN is pulled below 1.8 V , the module shuts down. A voltage between 2.0 V and 2.8 V selects the forced CCM mode which will run the module in continuous conduction at all times. A voltage higher than 3.1 V selects the DCM/CCM mode which will run the module in discontinuous conduction at light loads.

## Selecting the Forced CCM Mode

In order to set the module to operate in forced CCM, a voltage between 2.0 V and 2.8 V must be applied to EN/MODE. This can be achieved with an external control signal that meets the above voltage requirement. Where an external control is not available, the EN/MODE can be derived from $\mathrm{V}_{I N}$. If $\mathrm{V}_{\mathrm{IN}}$ is well regulated, use a resistor divider and set the voltage to 2.5 V . If $\mathrm{V}_{\mathrm{IN}}$ varies over a wide range, the circuit shown in Figure 25 can be used to generate the required voltage. Note that at $\mathrm{V}_{\mathrm{IN}}$ of 5.0 V and 40 V the nominal Zener voltage is 4.0 V and 5.0 V respectively. Therefore for $\mathrm{V}_{\mathrm{IN}}$ in the range of 5.0 V to 40 V , the circuit shown in Figure 25 will generate $\mathrm{V}_{\mathrm{EN}}$ required for forced CCM.

## Selecting the DCM/CCM Mode

In order to set the module operation to DCM/CCM, a voltage between 3.1 V and 5.5 V must be applied to EN/MODE pin. If an external control signal is available, it can be directly connected to EN/MODE. In applications where an external control is not available, EN/MODE input can be derived from $V_{I N}$. If $V_{I N}$ is well regulated, use a resistor divider and set the voltage to 4 V . If $\mathrm{V}_{\mathrm{IN}}$ varies over a wide range, the circuit shown in Figure 26 can be used to generate the required voltage for DCM/CCM operation.


Figure 25. Selecting Forced CCM by Deriving EN/MODE from $\mathrm{V}_{\mathrm{IN}}$


Figure 26. Selecting DCM/CCM by Deriving EN/MODE from $\mathrm{V}_{\mathrm{IN}}$

## Applications Information (Continued)

## Programming the On-Time

The on-time $\mathrm{t}_{\mathrm{ON}}$ is programmed via resistor $\mathrm{R}_{\mathrm{ON}}$ according to following equation:

$$
\mathrm{RON}_{\mathrm{O}}=\frac{\mathrm{V}_{\mathrm{IN}} \times\left[\mathrm{t} 0 \mathrm{~N}-\left(2.5 \times 10^{-8}\right)\right]}{2.95 \times 10^{-10}}
$$

A graph of ton vs. RON, using the above equation, is compared to typical test data in Figure 5. The graph shows that calculated data matches typical test data within $3 \%$.
The ton corresponding to a particular set of operating conditions can be calculated based on empirical data from:

$$
\mathrm{t}_{\mathrm{ON}}=\frac{\mathrm{V}_{\text {OUT }}}{\mathrm{V}_{\text {IN }} \times 1.06 \times \mathrm{f} \times \mathrm{Eff.}}
$$

Where:

- $f$ is the desired switching frequency at nominal lout
- Eff. is the converter efficiency corresponding to nominal lout
Substituting for $t_{0 N}$ in the first equation we get:

$$
\mathrm{R}_{\mathrm{ON}}=\frac{\left(\frac{\mathrm{V}_{\text {OUT }}}{1.06 \mathrm{xf} \times \text { Eff. }}\right)-\left[\left(2.5 \times 10^{-8}\right) \times \mathrm{V}_{\mathrm{IN}}\right]}{\left(2.95 \times 10^{-10}\right)}
$$

Now Ron can be calculated in terms of operating conditions $\mathrm{V}_{\text {IN }}, \mathrm{V}_{\text {OUT }}, \mathrm{f}$ and Eff. using the above equation. At $\mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}$, $f=500 \mathrm{kHz}$, $\mathrm{l}_{\text {OUt }}=3 \mathrm{~A}$ and using the efficiency numbers from Figure 22 we get the following $\mathrm{R}_{\mathrm{ON}}$ :

| $\mathrm{V}_{\text {OUT }}(\mathrm{V})$ | Eff. (\%) | $\mathrm{f}(\mathrm{kHZ})$ | $\mathrm{R}_{\text {ON }}(\mathrm{k} \Omega)$ |
| :---: | :---: | :---: | :---: |
| 12.0 | 94 | 700 | 56.3 |
| 5.0 | 90 | 500 | 33.5 |
| 3.3 | 87 | 500 | 22.2 |
| 1.8 | 80 | 500 | 12.4 |

## Overcurrent Protection (OCP)

If the load current exceeds the programmed overcurrent threshold locp for four consecutive switching cycles, the module enters the hiccup mode of operation. In hiccup mode the MOSFET gates are turned off for 110 ms (hiccup timeout). Following the hiccup timeout a soft-start is attempted. If OCP persists, hiccup timeout will repeat. The module will remain in hiccup mode until load current is reduced below the programmed locp. In order to program overcurrent protection use the following equation:

$$
\text { RLIM }=\left[\frac{(\mathrm{IOCP}+(0.5 \times \Delta \mathrm{I} \mathrm{~L}))}{\left(\frac{\mathrm{ILIM}}{\mathrm{RDS}}\right)}\right]+0.16 \mathrm{k} \Omega
$$

Where:

- $\mathrm{R}_{\text {LIM }}$ is resistor value in $k \Omega$ for programming loCP
- locp is the overcurrent value to be programmed
- $\Delta I_{L}$ is the peak-to-peak inductor current ripple
- $\mathrm{I}_{\mathrm{LIM}} / \mathrm{R}_{\mathrm{DS}}=2.4 \mu \mathrm{~A} / \mathrm{m} \Omega$ is the minimum value of the parameter specified in the tabulated data
- $0.16 \mathrm{k} \Omega$ accounts for OCP comparator offset

The above equation is for worst-case analysis and safeguards against premature OCP. Typical value of locp, for a given $\mathrm{R}_{\mathrm{LIM}}$, will be higher than that predicted by the above equation. Graph of calculated locp vs. $R_{\text {LIM }}$ is compared to typical locp in Figure 9.

## Short-Circuit Protection (SCP)

If the output voltage drops below $60 \%$ of its programmed value, the Module will enter hiccup mode. Hiccup will persist until short-circuit is removed. SCP circuit becomes active after PGOOD asserts high.

## Over Temperature Protection (OTP)

OTP triggers at a nominal controller temperature of $150^{\circ} \mathrm{C}$. The gate of switching FET and synchronous FET are turned off. When controller temperature cools down to $135^{\circ} \mathrm{C}$, soft-start is initiated and operation resumes.

## Applications Information (Continued)

## Programming the Output Voltage

Use an external voltage divider as shown in Figure 27 to program the output voltage $\mathrm{V}_{\text {OUT }}$.

$$
\mathrm{R}_{\mathrm{FB} 1}=\mathrm{R}_{\mathrm{FB} 2} \times\left(\frac{\mathrm{V}_{\text {OUT }}}{0.6 \mathrm{~V}}-1\right)
$$

Where $R_{\text {FB2 }}$ has a nominal value of $2 k \Omega$.

## Programming the Soft-Start

Place a capacitor $\mathrm{C}_{S S}$ between the SS and AGND pins to program the soft-start. In order to program a soft-start time of $t_{S S}$, calculate the required capacitance $\mathrm{C}_{S S}$ from the following equation:

$$
\mathrm{CSS}=\mathrm{tSS} \times \frac{10 \mu \mathrm{~A}}{0.6 \mathrm{~V}}
$$

## Feed-Forward Capacitor (CFF)

The feed-forward capacitor $C_{F F}$ is used to set the necessary phase margin when using ceramic output capacitors. Calculate $\mathrm{C}_{\mathrm{FF}}$ from the following equation:

$$
C_{F F}=\frac{1}{2 \times \pi \times R_{F B 1} \times 5 \times f L C}
$$

Where $f_{\text {LC }}$, the output filter double-pole frequency is calculated from:

$$
\mathrm{fLC}=\frac{1}{2 \times \pi \times \sqrt{\mathrm{LxC}} \mathrm{COT}}
$$

You must use manufacturer's DC derating curves to determine the effective capacitance corresponding to $\mathrm{V}_{\text {OUT }}$. A load step test and/or a loop frequency response test should be performed and if necessary C $_{\text {FF }}$ can be adjusted in order to get a critically damped transient load response.
In certain conditions an alternate compensation scheme may need to be employed using ripple injection from the inductor. An application note is being developed to provide more information about this compensation scheme.

## Feed-Forward Resistor ( $\mathrm{R}_{\mathrm{FF}}$ )

$R_{\mathrm{FF}}$, in conjunction with $\mathrm{C}_{\mathrm{FF}}$, functions similar to a high frequency pole and adds gain margin to the frequency response. Calculate $R_{\text {FF }}$ from:

$$
\mathrm{R}_{\mathrm{FF}}=\frac{1}{2 \times \pi \times f \times C_{\mathrm{FF}}}
$$

Where $f$ is the switching frequency.
If $R_{F F}>0.02 \times R_{F B 1}$ then calculate $R_{F F}$ value from $R_{F F}=0.02 \times R_{F B 1}$.

## Maximum Allowable Voltage Ripple at FB Pin

Note that the steady-state voltage ripple at feedback pin FB ( $\mathrm{V}_{\mathrm{FB}, \mathrm{RIPPLE}}$ ) must not exceed 50 mV in order for the module to function correctly. If $\mathrm{V}_{\mathrm{FB}, \mathrm{RIPPLE}}$ is larger than 50 mV then Cout should be increased as necessary in order to keep the $\mathrm{V}_{\mathrm{FB}, \mathrm{RIP} \text { PLE }}$ below 50 mV .

## Applications Information (Continued)



Figure 27. Typical Application Circuit

## Package Description

TOP VIEW
BOTTOM VIEW


SIDE VIEW


DETAIL A


All dimensions are in mm and angles in degrees.

## Package Description (Continued)

TERMINAL AND PAD EDGE DETAILS


## Package Description (Continued)

## RECOMMENDED STENCIL PATTERN



NOTE: Dashed line refers to stencil pattern.

## Package Description (Continued)

## RECOMMENDED LAND PATTERN



NOTE: Dashed line refers to land pattern.

## Ordering Information

| Part Number | Operating <br> Temperature Range | Environmental <br> Rating | Package | Packaging <br> Quantity | Marking |
| :--- | :---: | :---: | :---: | :---: | :---: |
| XR79203EL-F | $-40^{\circ} \mathrm{C} \leq T_{J} \leq 125^{\circ} \mathrm{C}$ | RoHS | $8 m \mathrm{~m} \times 8 \mathrm{~mm} \times 4 \mathrm{~mm}$ <br> QFN package | Tray | XR79203EL <br> YYWWF <br> XXXXXXXX |
| XR79203EVB | XR79203 evaluation board |  |  |  |  |

## NOTE:

$Y Y=$ Year, $W W=$ Work Week, $F=$ Lead Free and Halogen Free, $X X X X X X X X=$ Lot Number .


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