# $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator 

## General Description

The MAX44269 is an ultra-small and low-power dual comparator ideal for battery-powered applications such as cell phones, notebooks, and portable medical devices that have extremely aggressive board space and power constraints. The comparator is available in a miniature $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}, 9$-bump WLP package, making it the industry's smallest dual comparator.

The IC can be powered from supply rails as low as 1.8 V and up to 5.5 V . It requires just $0.5 \mu \mathrm{~A}$ of typical supply current per comparator. It has a rail-to-rail input structure and a unique output stage that limits supply current surges while switching. This design also minimizes overall power consumption under dynamic conditions. The IC has open-drain outputs, making it suitable for mixed voltage systems. The IC also features internal filtering to provide high RF immunity. It operates over a $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ temperature.

## Applications

Smartphones
Notebooks
Two-Cell Battery-Powered Devices
Battery-Operated Sensors
Ultra-Low-Power Systems
Portable Medical Mobile Accessories

Features

## - Ultra-Low Power Consumption $\diamond 0.5 \mu \mathrm{~A}$ per Comparator <br> - Ultra-Small 1.3mm x 1.3mm WLP Package <br> - Guaranteed Operation Down to $\mathrm{V}_{\mathrm{CC}}=1.8 \mathrm{~V}$ <br> - Input Common-Mode Voltage Range Extends 200mV Beyond-the-Rails <br> -6V Tolerant Inputs Independent of Supply <br> - Open-Drain Outputs <br> - Internal Filters Enhance RF Immunity <br> - Crowbar-Current-Free Switching <br> - Internal Hysteresis for Clean Switching <br> - No Output Phase Reversal for Overdriven Inputs

Ordering Information appears at end of data sheet.

For related parts and recommended products to use with this part, refer to www.maxim-ic.com/MAX44269.related.

Typical Application Circuit


A/AXI/VI Maxim Integrated Products
For pricing, delivery, and ordering information, please contact Maxim Direct at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.

# $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator 

## ABSOLUTE MAXIMUM RATINGS

| $V_{C C}$ to GND. | o +6V |
| :---: | :---: |
| INA+, INA-, INB+, INB- to GND | -0.3V to +6V |
| Continuous Input Current into Any Pin | $\ldots . . \pm 20 \mathrm{~mA}$ |
| Maximum Power Dissipation (derate $11.9 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ at $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ ). | $.952 \mathrm{~mW}$ |
| Output Voltage to GND (OUT_) | -0.3V to +6V |
| Output Current (OUT_) | $\ldots \pm 50 \mathrm{~mA}$ |

Output Short-Circuit Duration (OUT_) .......................Continuous Operating Temperature Range .......................... $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ Storage Temperature Range............................ $65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ Junction Temperature .................................................... $+150^{\circ} \mathrm{C}$
Lead Temperature (soldering, 10s) ................................ $+300^{\circ} \mathrm{C}$
Soldering Temperature (reflow) ...................................... $+260^{\circ} \mathrm{C}$

## PACKAGE THERMAL CHARACTERISTICS (Note 1)

WLP
Junction-to-Ambient Thermal Resistance ( $\theta_{\mathrm{JA}}$ ) .......... $84^{\circ} \mathrm{C} / \mathrm{W}$
Note 1: Package thermal resistances were obtained using the method described in JEDEC specification JESD51-7, using a fourlayer board. For detailed information on package thermal considerations, refer to www.maxim-ic.com/thermal-tutorial.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{GND}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{IN}+}=1.2 \mathrm{~V}, \mathrm{R}_{\text {PULLU }}=100 \mathrm{k} \Omega\right.$ to $\mathrm{V}_{\mathrm{CC}}, \mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.) (Note 2)

| PARAMETER | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DC CHARACTERISTICS |  |  |  |  |  |  |  |
| Input-Referred Hysteresis | $\mathrm{V}_{\mathrm{HYS}}$ | $\left(\mathrm{V}_{\mathrm{GND}}-0.2 \mathrm{~V}\right) \leq \mathrm{V}_{\mathrm{CM}} \leq\left(\mathrm{V}_{C C}+0.2 \mathrm{~V}\right)($ Note 3) |  |  | 4 | 6 | mV |
| Input Offset Voltage | Vos | $\begin{aligned} & \mathrm{V}_{\mathrm{GND}}-0.2 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CM}} \leq \\ & \mathrm{V}_{\mathrm{CC}}+0.2 \mathrm{~V}(\text { Note } 4) \end{aligned}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 0.15 | 5 | mV |
|  |  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C}$ |  |  | 10 |  |
| Input Bias Current | $I_{B}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | 0.15 |  | nA |
|  |  | $\mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |  | 0.2 |  |  |  |
| Output-Voltage Swing Low | VoL | $\mathrm{V}_{C C}=1.8 \mathrm{~V}$, | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 105 | 200 | mV |
|  |  | $\mathrm{I}_{\text {SINK }}=1 \mathrm{~mA}$ | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C}$ |  |  | 300 |  |
|  |  | $V_{C C}=5 \mathrm{~V}, \mathrm{I}_{\text {IINK }}=6 \mathrm{~mA}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 285 | 350 |  |
|  |  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C}$ | 450 |  |  |  |
| Input Voltage Range | $\mathrm{V}_{\mathrm{CM}}$ | Inferred from $\mathrm{V}_{\text {OS }}$ test |  | $\begin{aligned} & \mathrm{V}_{\mathrm{GND}} \\ & -0.2 \mathrm{~V} \end{aligned}$ |  | $\begin{array}{r} V_{\mathrm{CC}} \\ +0.2 \mathrm{~V} \end{array}$ | V |
| Output Short-Circuit Current | ISC | Sinking, $\mathrm{V}_{\text {OUT }}=\mathrm{V}_{\text {CC }}$ | $\mathrm{V}_{C C}=1.8 \mathrm{~V}$ |  | 3 |  | mA |
|  |  |  | $V_{C C}=5 \mathrm{~V}$ |  | 30 |  |  |
| Output Leakage Current | ILEAK | $\mathrm{V}_{C C}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=5.5 \mathrm{~V}$ |  |  | 0.2 |  | nA |

## $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator

## ELECTRICAL CHARACTERISTICS (continued)

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{GND}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=\mathrm{V}_{I N+}=1.2 \mathrm{~V}, \mathrm{R}_{\text {PULLU }}=100 \mathrm{k} \Omega\right.$ to $\mathrm{V}_{\mathrm{CC}}, \mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.) (Note 2)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AC CHARACTERISTICS |  |  |  |  |  |  |
| Propagation Delay High to Low (Note 5) | $t_{\text {PHL }}$ | Input overdrive $= \pm 100 \mathrm{mV}, \mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}$ |  | 5 |  | $\mu \mathrm{S}$ |
|  |  | Input overdrive $= \pm 100 \mathrm{mV}, \mathrm{V}_{C C}=1.8 \mathrm{~V}$ |  | 7 |  |  |
|  |  | Input overdrive $= \pm 20 \mathrm{mV}, \mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}$ |  | 8 |  |  |
|  |  | Input overdrive $= \pm 20 \mathrm{mV}, \mathrm{V}_{\mathrm{CC}}=1.8 \mathrm{~V}$ |  | 12 |  |  |
| Propagation Delay Low to High (Note 5) | tPLH | Input overdrive $= \pm 100 \mathrm{mV}, \mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}$ |  | 34 |  | $\mu \mathrm{s}$ |
|  |  | Input overdrive $= \pm 100 \mathrm{mV}, \mathrm{V}_{\mathrm{CC}}=1.8 \mathrm{~V}$ |  | 12 |  |  |
|  |  | Input overdrive $= \pm 20 \mathrm{mV}, \mathrm{V}_{C C}=5 \mathrm{~V}$ |  | 35 |  |  |
|  |  | Input overdrive $= \pm 20 \mathrm{mV}, \mathrm{V}_{\mathrm{CC}}=1.8 \mathrm{~V}$ |  | 12 |  |  |
| Fall Time | $\mathrm{t}_{\mathrm{F}}$ | $C_{\text {LOAD }}=15 \mathrm{pF}$ |  | 0.2 |  | $\mu \mathrm{s}$ |
| POWER SUPPLY |  |  |  |  |  |  |
| Supply Voltage Range | $\mathrm{V}_{\mathrm{CC}}$ | Guaranteed from PSRR tests | 1.8 |  | 5.5 | V |
| Power-Supply Rejection Ratio | PSRR | $\mathrm{V}_{\mathrm{CC}}=1.8 \mathrm{~V}$ to 5.5 V | 60 | 80 |  | dB |
| Supply Current per Comparator | ${ }^{\text {ICC }}$ | $\mathrm{V}_{C C}=1.8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 0.4 | 0.75 | $\mu \mathrm{A}$ |
|  |  | $V_{C C}=5 \mathrm{~V}, \mathrm{~T}_{A}=+25^{\circ} \mathrm{C}$ |  | 0.5 | 0.85 |  |
|  |  | $V_{C C}=5 \mathrm{~V},-40^{\circ} \mathrm{C} \leq \mathrm{T}_{A} \leq+85^{\circ} \mathrm{C}$ |  |  | 1 |  |
| Power-Up Time | ton |  |  | 1 |  | ms |

Note 2: All devices are $100 \%$ production tested at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$. Temperature limits are guaranteed by design.
Note 3: Hysteresis is the input voltage difference between the two switching points.
Note 4: $\mathrm{V}_{\mathrm{OS}}$ is the average of the positive and negative trip points minus $\mathrm{V}_{\mathrm{REF}}$.
Note 5: Overdrive is defined as the voltage above or below the switching points.

# $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator 

## Typical Operating Characteristics

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{GND}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=\mathrm{V}_{I N_{+}}=1.2 \mathrm{~V}, \mathrm{R}_{\mathrm{PULLUP}}=100 \mathrm{k} \Omega\right.$ to $\mathrm{V}_{\mathrm{CC}}, \mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted. All devices are $100 \%$ production tested at $T_{A}=+25^{\circ} \mathrm{C}$. Temperature limits are guaranteed by design.)


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## $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator

## Typical Operating Characteristics (continued)

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{GND}}=0 \mathrm{~V}, \mathrm{~V}_{I N-}=\mathrm{V}_{I N+}=1.2 \mathrm{~V}, \mathrm{R}_{\mathrm{PULLUP}}=100 \mathrm{k} \Omega\right.$ to $\mathrm{V}_{\mathrm{CC}}, \mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted. All devices are $100 \%$ production tested at $T_{A}=+25^{\circ} \mathrm{C}$. Temperature limits are guaranteed by design.)

$1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator

Typical Operating Characteristics (continued)
$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{GND}}=0 \mathrm{~V}, \mathrm{~V}_{I N-}=\mathrm{V}_{I N+}=1.2 \mathrm{~V}\right.$, RPULLUP $=100 \mathrm{k} \Omega$ to $\mathrm{V}_{\mathrm{CC}}, \mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted. All devices are $100 \%$ production tested at $T_{A}=+25^{\circ} \mathrm{C}$. Temperature limits are guaranteed by design.)



WLP

Bump Description

| PIN | NAME |  |
| :--- | :---: | :--- |
| A1 | INA- | Comparator A Inverting Input |
| A2 | INA+ | Comparator A Noninverting Input |
| A3 | OUTA | Comparator A Output |
| B1 | GND | Negative Supply Voltage. Bypass to GND with a 1.0нF capacitor. |
| B2 | N.C. | Not Connected |
| B3 | VCC | Positive Supply Voltage. Bypass to GND with a 1.0رF capacitor. |
| C1 | INB- | Comparator B Inverting Input |
| C2 | INB+ | Comparator B Noninverting Input |
| C3 | OUTB | Comparator B Output |

# $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator 

## Detailed Description

The MAX44269 is a general-purpose dual comparator for battery-powered devices where area, power, and cost constraints are crucial. The IC can operate with a low 1.8 V supply rail typically consuming $0.5 \mu \mathrm{~A}$ quiescent current per comparator. This makes it ideal for mobile and very low-power applications. The IC's common-mode input voltage range extends 200 mV beyond-the-rails. An internal 4 mV hysteresis ensures clean output switching, even with slow-moving input signals.

## Input Stage Structure

The input common-mode voltage range extends from $\left(V_{G N D}-0.2 \mathrm{~V}\right)$ to $\left(\mathrm{V}_{\mathrm{CC}}+0.2 \mathrm{~V}\right)$. The comparator operates at any different input voltage within these limits with low input bias current. Input bias current is typically $0.15 n A$ if the input voltage is between the supply rails.
The IC features a unique input ESD structure that can handle voltages from -0.3 V to 6 V independent of supply voltage. This allows for the device to be powered down with a signal still present on the input without damaging the part. This feature is useful in applications where one of the inputs has transient spikes that exceed the supply rails.

## No Output Phase Reversal for Overdriven Inputs

The IC's design is optimized to prevent output phase reversal if both the inputs are within the input common mode voltage range. If one of the inputs is outside the input common-mode voltage range, then output phase reversal does not occur as long as the other input is kept within the valid input common-mode voltage range. This behavior is shown in the No Output Phase Reversal graph in the Typical Operating Characteristics section.

## Open-Drain Output

The IC features an open-drain output, enabling greater control of speed and power consumption in the circuit design. The output logic level is also independent from the input, allowing for simple level translation.

## RF Immunity

The IC has very high RF immunity due to on-chip filtering of RF sensitive nodes. This allows the IC to hold its output state even in the presence of high amounts of RF noise. This improved RF immunity makes the IC ideal for mobile wireless devices.

Applications Information

## Hysteresis

Many comparators oscillate in the linear region of operation because of noise or undesired parasitic feedback. This tends to occur when the voltage on one input is equal or very close to the voltage on the other input.
The hysteresis in a comparator creates two trip points: one for the rising input voltage and one for the falling input voltage (Figure 1). The difference between the trip points is the hysteresis. When the comparator's input voltages are equal and the output trips, the hysteresis effectively causes one comparator input to move quickly past the other. This takes the input out of the region where oscillation occurs. This provides clean output transitions for noisy, slow-moving input signals. The IC has an internal hysteresis of 4 mV . Additional hysteresis can be generated with three resistors using positive feedback (Figure 2).


Figure 1. Threshold Hysteresis Band (Not to Scale)


Figure 2. Adding Hysteresis with External Resistors

# $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator 

Use the following procedure to calculate resistor values.

1) Select R3. Input bias current at $I_{-}+$is less than $15 n A$. To minimize errors caused by the input bias current, the current through R3 should be at least $1.5 \mu \mathrm{~A}$. Current through R3 at the trip point is ( $\left.V_{\text {REF }}-V_{\text {OUT }}\right)$ / R3. Considering the two possible output states in solving for R3 yields two formulas:

$$
R 3=V_{R E F} / I R 3 \text { and } R 3=\left[\left(V_{C C}-V_{R E F}\right) / I R 3\right]-R 1
$$

Use the smaller of the two resulting resistor values. For example, for $\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}$, $\mathrm{IR} 3=-1.5 \mu \mathrm{~A}, \mathrm{R} 1=200 \mathrm{k} \Omega$, and a $V_{\text {REF }}=1.24 \mathrm{~V}$, the two resistor values are $827 \mathrm{k} \Omega$ and $1.5 \mathrm{M} \Omega$. Therefore, for R3 choose the standard value of $825 \mathrm{k} \Omega$.
2) Choose the hysteresis band required $\left(\mathrm{V}_{\mathrm{HB}}\right)$. In this example, the $\mathrm{V}_{\mathrm{HB}}=50 \mathrm{mV}$.
3) Calculate R2 according to the following equation:

$$
R 2=(R 1+R 3)\left(\frac{V_{H B}}{V_{C C}+\left(V_{R E F} \times R 1\right) / R 3}\right)
$$

For this example, insert the value:

$$
\mathrm{R} 2=(200 \mathrm{k} \Omega+0.825 \mathrm{M} \Omega)\left(\frac{50 \mathrm{mV}}{5.3}\right)=9.67 \mathrm{k} \Omega
$$

For this example, choose standard value $\mathrm{R} 2=9.76 \mathrm{k} \Omega$.
4) Choose the trip point for $\mathrm{V}_{I N}$ rising $\left(\mathrm{V}_{\mathrm{THR}}\right)$ in such a way that:

$$
\mathrm{V}_{\mathrm{THR}}>\mathrm{V}_{\mathrm{REF}}\left(1+\frac{\mathrm{V}_{\mathrm{HB}}}{\mathrm{~V}_{\mathrm{CC}}}\right)
$$

$V_{\text {THR }}$ is the threshold voltage at which the comparator switches its output from low to high, as $\mathrm{V}_{\mathrm{IN}}$ rises above the trip point. For this example, choose $V_{T H R}=3 V$.
5) Calculate R4 as follows:

$$
\begin{gathered}
R 4=\frac{1}{\left(\frac{V_{T H R}}{V_{R E F} \times R 2}\right)-\left(\frac{1}{R 2}\right)-\left(\frac{1}{R 3}\right)} \\
R 4=\frac{1}{\left(\frac{3}{1.24 \times 9.76}\right)-\left(\frac{1}{9.76}\right)-\left(\frac{1}{825}\right)}=6.93 \mathrm{k} \Omega
\end{gathered}
$$

For this example, choose a standard value of $6.98 \mathrm{k} \Omega$.
6) Verify the trip voltages and hysteresis as follows:

$$
\begin{aligned}
& \mathrm{V}_{\mathrm{THR}}=\mathrm{V}_{\mathrm{REF}} \times R 2\left(\left(\frac{1}{\mathrm{R} 2}\right)+\left(\frac{1}{\mathrm{R} 3}\right)+\left(\frac{1}{\mathrm{R} 4}\right)\right) \\
& \mathrm{V}_{\mathrm{THF}}=\mathrm{V}_{\mathrm{REF}} \times R 2\left(\left(\frac{1}{\mathrm{R} 2}\right)+\left(\frac{1}{\mathrm{R} 1+\mathrm{R} 3}\right)+\left(\frac{1}{\mathrm{R} 4}\right)\right) \\
& -\frac{\mathrm{R} 2}{\mathrm{R} 1+\mathrm{R} 3} \times \mathrm{V}_{\mathrm{CC}}
\end{aligned}
$$

The hysteresis network in Figure 2 can be simplified if the reference voltage is chosen to be at midrail and the trip points of the comparator are chosen to be symmetrical about the reference voltage. Use the circuit in Figure 3 if the reference voltage can be designed to be at the center of the hysteresis band. For the symmetrical case, follow the same steps outlined in the paragraph above to calculate the resistor values except that in this case, resistor R4 approaches infinity (open). So in the previous example with $\mathrm{V}_{\mathrm{REF}}=2.5 \mathrm{~V}$, if $\mathrm{V}_{\mathrm{THR}}=2.525 \mathrm{~V}$ and $\mathrm{V}_{\mathrm{THF}}$ $=2.475 \mathrm{~V}$ then using the above formulas, we get $\mathrm{R} 1=$ $200 \mathrm{k} \Omega, \mathrm{R} 2=9.09 \mathrm{k} \Omega$ and $\mathrm{R} 3=825 \mathrm{k} \Omega, \mathrm{R} 4=$ not installed.

## Jack Detect

The IC can be used to detect peripheral devices connected to a circuit. This includes a simple jackdetect scheme for cell phone applications. The Typical Application Circuit shows how the device can be used in conjunction with an external reference to detect a remote key connection and an accessory ID input. The opendrain output of the devices allows the output logic level to be controlled independent of the peripheral device's load, making interfacing and controlling external devices as simple as monitoring a few digital inputs on a microcontroller or codec.


Figure 3. Simplified External Hysteresis Network if $V_{R E F}$ is at the Center of the Hysteresis Band

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## Logic-Level Translator

Due to the open-drain output of the IC, the device can translate between two different logic levels (Figure 4). If the internal 4 mV hysteresis is not sufficient, then external resistors can be added to increase the hysteresis as shown in Figure 2 and Figure 3.

Power-On Reset Circuit
The IC can be used to make a power-on reset circuit as displayed in Figure 5. The positive input provides the ratiometric reference with respect to the power supply and is created by a simple resistive divider. Choose reasonably large values to minimize the power consumption in the resistive divider. The negative input provides the power-on delay time set by the time constant of the RC circuit formed by R2 and C1. This simple circuit can be used to power up the system in a known state after ensuring that the power supply is stable. Diode D1 provides a rapid reset in the event of unexpected power loss.


Figure 4. Logic-Level Translator


Figure 5. Power-On Reset Circuit

Relaxation Oscillator
The IC can also be used to make a simple relaxation oscillator (Figure 6). By adding the RC circuit R5 and C1, a standard Schmidt Trigger circuit referenced to a set voltage is converted into an astable multivibrator. As shown in Figure 7, IN - is a sawtooth waveform with capacitor C1 alternately charging and discharging through resistor R5. The external hysteresis network formed by R1 to R4 defines the trip voltages as:

$$
\begin{aligned}
& V_{T_{-} \text {RISE }}=V_{C C}\left(\frac{R 3 \times R 4}{R 2 R 3+R 2 R 4+R 3 R 4}\right) \\
& V_{T_{-}} F A L L=V_{C C}\binom{R 4 R 5(R 1+R 2+R 3)}{+R 1 R 3 R 4}
\end{aligned}
$$

Using the basic time domain equations for the charging and discharging of an RC circuit, the logic-high time, logic-low time, and frequency can be calculated as:

$$
\text { tLow }=R 5 C 1 \ln \left(\frac{V_{T} \text { FALL }}{V_{T_{-}} \text {RISE }}\right)
$$



Figure 6. Relaxation Oscillator

# $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator 

Since the comparator's output is open drain, it goes to high impedance corresponding to logic-high. So, when the output is at logic-high, the C1 capacitor charges through the resistor network formed by R1 to R5 as shown in Figure 8. An accurate calculation of tHIGH would have involved applying thevenin's theorem to compute the equivalent thevenin voltage ( $\mathrm{V}_{\text {THEVENIN }}$ ) and thevenin resistance (RTHEVENIN) in series with the capacitor C1. thigh can then be computed using the basic time domain equations for the charging RC circuit as:

$$
\begin{gathered}
\text { tHIGH }=R_{\text {THEVENIN }} C 1 \ln \left(\frac{V_{\text {THEVENIN }}-V_{T_{\_} R I S E}}{V_{\text {THEVENIN }}-V_{T_{-}} \text {FALL }}\right) \\
R_{\text {THEVENIN }}=[(R 2 \| R 4)+R 3] \| R 1+R 5 \\
V_{\text {THEVENIN }}= \\
=\frac{V_{C C}[(R 2 \| R 4)+R 3]}{(R 2 \| R 4)+R 3+R 1}+\frac{V_{C C} \times R 4}{R 2+R 4} \\
\times \frac{R 1}{(R 2 \| R 4)+R 3+R 1}
\end{gathered}
$$

The $t_{\text {HIGH }}$ calculation can be simplified by selecting the component values in such a way that R3 >> R1 and R5 >> R1. This ensures that the output of the comparator goes close to $\mathrm{V}_{\mathrm{CC}}$ when at logic-high (that is, $\mathrm{V}_{\text {THEVENIN }}$ $\sim V_{\text {CC }}$ and RTHEVENIN ~ R5). With this selection, $\mathrm{t}_{\text {HIGH }}$ can be approximated as:

$$
\mathrm{tHIGH}=\mathrm{R} 5 \mathrm{C} 1 \ln \left(\frac{\mathrm{~V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{T}} \_\mathrm{RISE}}{\mathrm{~V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{T}} \mathrm{FALL}}\right)
$$



Figure 7. Relaxation Oscillator Waveforms

The frequency of the relaxation oscillator is:

$$
\mathrm{f}=\frac{1}{\text { tHIGH }+ \text { tLOW }}=\frac{1}{R 5 C 11 n\left(\frac{\mathrm{~V}_{T_{-} \text {FALL }}\left(\mathrm{V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{T}_{-} R I S E}\right)}{\mathrm{V}_{\mathrm{T}_{-} R I S E}\left(\mathrm{~V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{T}_{-} \mathrm{FALL}}\right)}\right)}
$$

Simple PWM Generation Circuit
A pulse-width modulated (PWM) signal generator can be made utilizing both comparators in the IC (Figure 9). The capacitor/feedback resistor combination on INA- determines the switching frequency and the analog control voltage determines the pulse width.


Figure 8. Charging Network Corresponding to Logic-High Output


Figure 9. PWM Generator

# $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator 

## Window Detector Circuit

The IC is ideal for window detectors (undervoltage/overvoltage detectors). Figure 10 shows a window detector circuit for a single-cell Li+ battery with a 2.9 V end-of-life charge, a peak charge of 4.2 V , and a nominal value of 3.6V. Choose different thresholds by changing the values of R1, R2, and R3. OUTA provides an active-low undervoltage indication, and OUTB provides an active-low overvoltage indication. The open-drain outputs of both the comparators are wired OR to give an active-high power-good signal.
The design procedure is as follows:

1) Select R1. The input bias current into INB- is less than 15 nA , so the current through R1 should exceed $1.5 \mu \mathrm{~A}$ for the thresholds to be accurate. In this example, choose R1 $=825 \mathrm{k} \Omega(1.24 \mathrm{~V} / 1.5 \mu \mathrm{~A})$.
2) Calculate R2 + R3. The overvoltage threshold should be 4.2 V when $\mathrm{V}_{\text {IN }}$ is rising. The design equation is as follows:

$$
\begin{aligned}
R 2+R 3 & =R 1 \times\left[\left(\frac{V_{\mathrm{OTH}}}{\mathrm{~V}_{\mathrm{REF}}}\right)-1\right] \\
& =825 \times\left[\left(\frac{4.2}{1.24}\right)-1\right] \\
& =1969 \mathrm{k} \Omega
\end{aligned}
$$

3) Calculate R2. The undervoltage threshold should be 2.9 V when $\mathrm{V}_{\mathrm{IN}}$ is falling. The design equation is as follows:

$$
\begin{aligned}
& R 2=(R 1+R 2+R 3) \times\left(\frac{V_{\text {REF }}}{V_{\text {UTH }}}\right)-R 1 \\
= & ((825+1969) \times(1.24 / 2.9))-825 \\
= & 370 \mathrm{k} \Omega
\end{aligned}
$$

For this example, choose a $374 \mathrm{k} \Omega$ standard value $1 \%$ resistor.
4) Calculate R3:

$$
\begin{gathered}
R 3=(R 2+R 3)-R 2 \\
=1969 \mathrm{k} \Omega-374 \mathrm{k} \Omega \\
=1.595 \mathrm{M} \Omega
\end{gathered}
$$

For this example, choose a $1.58 \mathrm{M} \Omega$ standard value $1 \%$ resistor.

Board Layout and Bypassing
Use $1.0 \mu \mathrm{~F}$ bypass capacitors from $\mathrm{V}_{\mathrm{CC}}$ to GND. To maximize performance, minimize stray inductance by putting this capacitor close to the $\mathrm{V}_{\mathrm{CC}}$ pin and reducing trace lengths.


Figure 10. Window Detector Circuit
Chip Information
PROCESS: BiCMOS

Ordering Information

| PART | TEMP RANGE | PIN- <br> PACKAGE | TOP <br> MARK |
| :---: | :---: | :---: | :---: |
| MAX44269EWL +T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 9 WLP | +AJL |

+Denotes a lead(Pb)-free/RoHS-compliant package. $T=$ Tape and reel.

## $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power <br> Dual Comparator

Package Information
For the latest package outline information and land patterns (footprints), go to www.maxim-ic.com/packages. Note that a "+", "\#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

| PACKAGE TYPE | PACKAGE CODE | OUTLINE NO. | LAND PATTERN NO. |
| :---: | :---: | :---: | :---: |
| 9 WLP | W91B1-6 | $\underline{21-0430}$ | Refer to Application Note 1891 |


$\qquad$

# $1.3 \mathrm{~mm} \times 1.3 \mathrm{~mm}$, Low-Power Dual Comparator 

Revision History

| REVISION <br> NUMBER | REVISION <br> DATE | DESCRIPTION | PAGES <br> CHANGED |
| :---: | :---: | :--- | :---: |
| 0 | $9 / 11$ | Initial release | - |
| 1 | $12 / 11$ | Revised Electrical Characteristics, Typical Operating Characteristics, and Figure 5. | $3,5,6,9,10$ |

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